

Full-vectorial modal analysis for circular optical waveguides based on the multidomain Chebyshev pseudospectral method

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What we believe to be a new one-dimensional full-vectorial mode solver for circular waveguides in step-index optical fibers is introduced based on the multidomain Chebyshev pseudospectral method and the perfectly matched layer. The formulations are derived with two transverse components on the radial axis in the cylindrical coordinate system. The electromagnetic fields are expanded inside each homogeneous layer by the Chebyshev basis functions, and then matched rigorously at the radial discontinuities by the interface conditions. The numerical analysis on the guided and leaky modes of the two layer **air-clad fiber, hybrid surface plasmon polariton, and Bragg fibers** demonstrates the validity and good performance of the present method, which has remarkably high accuracy and fast convergence. © 2010 Optical Society of America

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1. INTRODUCTION

The accurate calculation of full-vectorial modes of circular optical waveguides is important for the design and application of such waveguide structures in certain optical devices. In the past few decades, many numerical methods [1–7] have been proposed and widely used to solve this problem. The finite difference (FD) method is one of the most popular methods for its simplicity and flexibility. As known, one major difficulty in the FD methods is how to handle the interface conditions at the index discontinuities without losing the whole solution accuracy [4,8]. It has been verified in [8] that the commonly used average-index approximation in the conventional FD schemes has only zero-order truncation error at the interface points in the Cartesian coordinate. Recently, Lu *et al.* introduced a second order one-dimensional (1-D) full-vectorial FD mode solver [4] for circular optical waveguides. Their FD formulations are described with two transverse components H_r - H_ϕ on the radial axis in the cylindrical coordinate system, where the angular variable is separated due to the circular symmetry. In this method, the fields are rigorously matched at the radial discontinuities by the use of Taylor expansion, and the resultant matrix still keeps its compact form. Inside each homogeneous layer, the vectorial wave equations are discretized by the central FD scheme. Consequently, this FD method has second order accuracy overall. However, such a precision is still not high enough, especially in some large structures, where a great number of nodes will be needed due to the low accuracy of FD methods. Therefore, higher order methods are still important to further improve the efficiency and accuracy.

In recent years, the pseudospectral method [9–13], also called the spectral collocation method (SCM), has attracted more and more attention in computational elec-

tromagnetics (CEM) due to its high accuracy and fast convergence over the conventional methods. There is an excellent book [14] introducing this method. As known, the high order accuracy of spectral methods relies on the smoothness of solution functions [14]. Thus, a proper treatment of the interface conditions is also crucial for the spectral methods applied in CEM. In [15], Huang *et al.* first employed the multidomain pseudospectral method to analyze the modes of dielectric waveguides with step-index profiles. Their two-dimensional (2-D) formulations are introduced with two transverse components H_x - H_y in the rectangular coordinate system. In their method, the domain is divided into several subdomains with homogeneous refractive indices. The fields in each subdomain are approximated independently by the SCM and finally connected rigorously by matching the interface conditions between the adjacent subdomains. This method has been verified to own spectral accuracy. However, it can only be used in problems with horizontal and vertical interfaces. Chiang *et al.* then proposed another multidomain pseudospectral frequency-domain (PSFD) scheme in [6] to determine the guided modes of general 2-D optical waveguides with arbitrary interfaces. The formulations of the PSFD method are described by H_ξ - H_η in the curvilinear coordinate system. Furthermore, they also analyzed the leaky modes in [7] by incorporating the perfectly matched layer (PML) [16] with the PSFD. However, the PSFD method is not so efficient for circular optical waveguides because it does not take use of the circular symmetry.

In this study, we show the details for the first time to apply the multidomain Chebyshev pseudospectral (MCPS) method to solve the same 1-D full vectorial modal equations as in [4] under the cylindrical coordinate system. In our method, the electromagnetic fields are ex-

panded inside each homogeneous layer on the radial axis by the Chebyshev basis functions, and then matched rigorously at the radial discontinuities by the interface conditions. The PML [4,17,18] in the cylindrical coordinate system is also applied to accurately determine the guided and leaky modes. Furthermore, the generalized matrix eigenvalue problem obtained by MCPS is finally transformed into a standard one, which can be solved easily by common matrix eigenvalue solvers. The numerical analysis of the two layer air-clad fiber [6,19], hybrid surface plasmon polaritons (SPPs) [20,21], and Bragg fibers [4,22–24] shows the validity and excellent performance of our method.

This paper is organized as follows. In Section 2, we formulate the modal equations of circular optical fibers. The MCPS scheme is introduced in Section 3. Then it is validated in Section 4 by various numerical examples. Finally, we conclude this paper in Section 5.

2. PROBLEM FORMULATION

A quarter of the cross section of one step-index circular optical fiber is shown in Fig. 1, where the fiber is composed of piecewise homogeneous layers with refractive index n_i ($i=1,2,\dots,N$). The radial discontinuities are denoted as r_i for $i=1,2,\dots,N-1$. Notice that the outmost infinite cladding layer with n_N is enclosed at r_N by the PML and r_{pml} is the radius of the physical region. Thus, the thickness of the PML is $d=r_N-r_{\text{pml}}$.

The 1-D modal equations, interface, and boundary conditions for the circular waveguide were proposed in [3,4]. We also briefly introduce them here. They are expressed by the magnetic field vector $\mathbf{H}=[H_r \ H_\phi \ H_z]^T$, and the electric formulations with $\mathbf{E}=[E_r \ E_\phi \ E_z]^T$ can be obtained by a small modification on the interface conditions.

Suppose that \mathbf{H} is time-harmonic and propagates along the longitudinal z -direction. Then it satisfies

$$\mathbf{H}(r, \phi, z) = \begin{bmatrix} H_r(r) \cos(m\phi) \\ H_\phi(r) \sin(m\phi) \\ H_z(r, \phi) \end{bmatrix} \exp[j(\omega t - \beta z)], \quad (1)$$

where $m=0,1,2,\dots$ is the angular separation constant, t

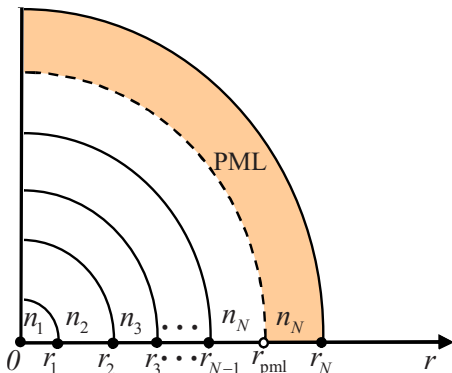


Fig. 1. (Color online) A quarter of the cross section of a step-index circular fiber.

is the time variable, ω is the wave frequency, and β is the unknown propagation constant.

As seen in [3,4], in the frequency domain, after reducing H_z from

$$\nabla \times (\nabla \times \mathbf{H}) = \kappa_0^2 \epsilon_r \mathbf{H},$$

and separating variables ϕ and z , we get the full-vectorial modal equations for circular waveguides only with the radial variable r ,

$$\left(\frac{d^2}{dr^2} + \frac{1}{r} \frac{d}{dr} + \kappa_0^2 \epsilon_r + \frac{M}{r^2} \right) \begin{bmatrix} H_r \\ H_\phi \end{bmatrix} = \beta^2 \begin{bmatrix} H_r \\ H_\phi \end{bmatrix}, \quad (2)$$

where κ_0 is the wavenumber of free space, ϵ_r is the relative permittivity, and

$$M = - \begin{bmatrix} m^2 + 1 & 2m \\ 2m & m^2 + 1 \end{bmatrix}.$$

For simplicity, we denote the transverse magnetic field $\begin{bmatrix} H_r \\ H_\phi \end{bmatrix}$ as \mathbf{H} and the transverse electric field $\begin{bmatrix} E_r \\ E_\phi \end{bmatrix}$ as \mathbf{E} hereafter.

As known, \mathbf{H} needs to satisfy the interface conditions [4] at the radial discontinuity r_i , with $i=1,2,\dots,N-1$. Namely,

$$\mathbf{H}(r_i^-) = \mathbf{H}(r_i^+), \quad (3)$$

$$\frac{d\mathbf{H}(r_i^-)}{dr} = \frac{(\epsilon_{r_i^-}/\epsilon_{r_i^+} - 1)}{r_i} \begin{bmatrix} 0 & 0 \\ m & 1 \end{bmatrix} \mathbf{H}(r_i^+) + \begin{bmatrix} 1 & 0 \\ 0 & \epsilon_{r_i^-}/\epsilon_{r_i^+} \end{bmatrix} \frac{d\mathbf{H}(r_i^+)}{dr}, \quad (4)$$

where $\epsilon_{r_i^-}$ and $\epsilon_{r_i^+}$ denote the permittivities of the inner and outer media at r_i , respectively. These two equations are derived from the continuities of the tangential fields H_z and E_z .

Obviously, a singularity exists at $r=0$ in Eq. (2). This is caused by the inherent property of the cylindrical coordinate system. The fields are actually bounded and smooth at this pole. So an additional boundary condition is set at $r=0$. Namely,

$$\mathbf{H} = 0, \quad m \neq 1, \quad (5)$$

$$\frac{d\mathbf{H}}{dr} = 0, \quad m = 1, \quad (6)$$

at $r=0$ (see [4]).

At last, we add the PML to this model. This is done by taking a complex coordinate transform [4,17,18] on the radial variable r in Eq. (2). There are

$$\frac{1}{s^2(r)} \frac{d^2 H_r}{dr^2} + \left(\frac{1}{s(r)} \frac{d}{dr} \left(\frac{1}{s(r)} \right) + \frac{1}{\hat{r}s(r)} \right) \frac{dH_r}{dr} + \left(\kappa^2 \varepsilon_r - \frac{m^2 + 1}{\hat{r}^2} \right) H_r - \frac{2m}{\hat{r}^2} H_\phi = \beta^2 H_r, \quad (7)$$

$$\frac{1}{s^2(r)} \frac{d^2 H_\phi}{dr^2} + \left(\frac{1}{s(r)} \frac{d}{dr} \left(\frac{1}{s(r)} \right) + \frac{1}{\hat{r}s(r)} \right) \frac{dH_\phi}{dr} + \left(\kappa^2 \varepsilon_r - \frac{m^2 + 1}{\hat{r}^2} \right) H_\phi - \frac{2m}{\hat{r}^2} H_r = \beta^2 H_\phi, \quad (8)$$

where

$$\hat{r} = \int_0^r s(t) dt, \quad s(r) = \frac{\partial \hat{r}}{\partial r} = \begin{cases} 1, & r < r_{\text{pml}} \\ 1 - j \frac{\sigma_r}{\omega \varepsilon_0 \varepsilon_r}, & r > r_{\text{pml}}, \end{cases} \quad (9)$$

with $\sigma_r = \sigma_{r,\text{max}} |r - r_{\text{pml}}|^P / d^P$ and P is a positive number. The maximum conductivity $\sigma_{r,\text{max}}$ can be determined by the reflection coefficient R [25], i.e.,

$$\sigma_{r,\text{max}} = \frac{(P+1)\varepsilon_r}{2\eta_0 d} \ln \frac{1}{R}, \quad (10)$$

where η_0 is the wave impedance in free space.

As shown in [4,18,26], the PML in Eq. (9) cannot absorb the evanescent waves. One way to overcome this difficulty is to make σ_r complex. But it will make the propagating waves oscillate faster, which exacerbates the numerical reflection [27]. Another way is to set the computational domain large enough and the evanescent waves will decay naturally. For simplicity, this paper chooses the second approach.

The zero Dirichlet boundary condition,

$$\mathbf{H}(r_N) = 0, \quad (11)$$

is set on the outer boundary of the PML. Thus, the total modal equations denoted by \mathbf{H} for the circular fiber are composed of Eqs. (3)–(8) and (11). And the solution domain is the closed segment $[r_0, r_N]$, where $r_0 = 0$.

The \mathbf{E} modal equations have the same form as \mathbf{H} except the interface conditions (3) and (4) are replaced with

$$\mathbf{E}(r_i^-) = \begin{bmatrix} \varepsilon_{r_i^+}/\varepsilon_{r_i^-} & 0 \\ 0 & 1 \end{bmatrix} \mathbf{E}(r_i^+), \quad (12)$$

$$\frac{d\mathbf{E}(r_i^-)}{dr} = \frac{(1 - \varepsilon_{r_i^+}/\varepsilon_{r_i^-})}{r_i} \begin{bmatrix} 1 & 0 \\ m & 0 \end{bmatrix} \mathbf{E}(r_i^+) + \frac{d\mathbf{E}(r_i^+)}{dr}; \quad (13)$$

see [4].

3. THE MCPS METHOD FOR CIRCULAR FIBER

A. Chebyshev Differentiation Matrix

We first introduce the definition of the Chebyshev differentiation matrix [14], which is important in the Chebyshev pseudospectral method. In $[-1, 1]$, the smooth function $f(x)$ can be approximated by

$$f(x) \approx \sum_{i=0}^q f(x_i) g_i(x), \quad (14)$$

where $g_i(x)$ is the Chebyshev–Lagrange interpolating polynomial of degree q , satisfying

$$g_i(x) = \frac{(1-x^2)T'_q(x)(-1)^{i+1}}{c_i q^2 (x-x_i)}, \quad (15)$$

with $c_0 = c_q = 2$ and $c_i = 1$ for $1 \leq i \leq q-1$. The polynomial $T_q(x)$ in Eq. (15) is defined by $T_q(x) = \cos(q \cos^{-1}(x))$, where $|x| \leq 1$. The node $x_i = \cos(i\pi/q)$ is the so called Chebyshev–Gauss–Lobatto point, which is also the root of $(1-x^2)T'_q(x)$.

The first order Chebyshev differentiation matrix $D_1 = (d_{i,j})_{(q+1) \times (q+1)}$ on a general segment $[a, b]$ satisfies

$$\begin{bmatrix} f'(t_0) \\ f'(t_1) \\ \vdots \\ f'(t_q) \end{bmatrix} \approx D_1 \begin{bmatrix} f(t_0) \\ f(t_1) \\ \vdots \\ f(t_q) \end{bmatrix}, \quad (16)$$

where

$$t_k = a + \frac{b-a}{2}(1-x_k), \quad k = 0, 1, \dots, q. \quad (17)$$

Thus, $t_0 = a$ and $t_q = b$. The matrix D_1 in Eq. (16) can be calculated by

$$d_{i,j} = -\frac{2}{b-a} \begin{cases} \frac{c_i}{c_j} \frac{(-1)^{i+j}}{x_i - x_j}, & i \neq j \\ \frac{-x_i}{2(1-x_i^2)}, & 1 \leq i = j \leq q-1 \\ \frac{2q^2+1}{6}, & i = j = 0 \\ -\frac{2q^2+1}{6}, & i = j = q \end{cases}; \quad (18)$$

see [28]. Similarly, the second order Chebyshev differentiation matrix D_2 satisfies

$$\begin{bmatrix} f''(t_0) \\ f''(t_1) \\ \vdots \\ f''(t_q) \end{bmatrix} \approx D_2 \begin{bmatrix} f(t_0) \\ f(t_1) \\ \vdots \\ f(t_q) \end{bmatrix},$$

and it can be easily calculated by $D_2 = D_1^2$.

B. Discretizations of the Modal Equations by the MCPS Method

In the MCPS method, the domain $[r_0, r_N]$ is divided into subdomains $\{[r_{i-1}, r_i]\}_{i=1}^N$, where the index n_i is constant in $[r_{i-1}, r_i]$ for $i=1, 2, \dots, N$. Suppose the degree of the Chebyshev–Lagrange interpolating polynomial on the i th segment $[r_{i-1}, r_i]$ is q_i , the corresponding first and second order Chebyshev differentiation matrices are $D_1^{(i)}$ and $D_2^{(i)}$, and the discrete nodes are $\{t_k^{(i)}\}_{k=0}^{q_i}$ with $t_0^{(i)} = r_{i-1}$ and $t_{q_i}^{(i)} = r_i$. Let \mathbf{H}_i and $\bar{\mathbf{H}}_i$ be

$$\mathbf{H}_i = [H_r(t_0^{(i)}) \ H_r(t_1^{(i)}) \ \cdots \ H_r(t_{q_i}^{(i)}) \ H_\phi(t_0^{(i)}) \ H_\phi(t_1^{(i)}) \ \cdots \ H_\phi(t_{q_i}^{(i)})]^T, \quad (19)$$

$$\bar{\mathbf{H}}_i = [H_r(t_1^{(i)}) \ H_r(t_2^{(i)}) \ \cdots \ H_r(t_{q_i-1}^{(i)}) \ H_\phi(t_1^{(i)}) \ H_\phi(t_2^{(i)}) \ \cdots \ H_\phi(t_{q_i-1}^{(i)})]^T. \quad (20)$$

The discretizations are based on the Chebyshev differentiation matrix defined before. Firstly, the modal equations (7) and (8) at $\{t_k^{(i)}\}_{k=1}^{q_i-1}$ in (r_{i-1}, r_i) are discretized to

$$\begin{bmatrix} A_i & B_i \\ B_i & A_i \end{bmatrix} \mathbf{H}_i = \beta^2 \bar{\mathbf{H}}_i, \quad (21)$$

where

$$A_i = \text{diag}\left(\frac{1}{s^2(t_k^{(i)})}\right) D_2^{(i)}(2:q_i, :) + \text{diag}\left(\frac{p_k}{s(t_k^{(i)})} + \frac{1}{\hat{r}_k s(t_k^{(i)})}\right) D_1^{(i)} \\ \times (2:q_i, :) + \text{diag}\left(\kappa_0^2 \varepsilon_r - \frac{m^2 + 1}{\hat{r}_k}\right), \\ B_i = \text{diag}\left(\frac{2m}{\hat{r}_k}\right),$$

with $p_k = (d/dr)[1/s(r)]|_{r_k^{(i)}}$ and $\hat{r}_k = \hat{r}|_{r_k^{(i)}}$ for $k=1, 2, \dots, q_i-1$. Here $\text{diag}(w_k)$ indicates the diagonal matrix with $\{w_k\}$ as the principal diagonal elements, and $D_j^{(i)}(2:q_i, :)$ is a MATLAB notation denoting the matrix obtained from eliminating the first and last rows of $D_j^{(i)}$ ($j=1, 2$).

Secondly, the interface conditions in Eqs. (3) and (4) are discretized at $r_i = t_{q_i}^{(i)}$. The Dirichlet equation (3) is discretized to

$$\mathbf{H}(t_{q_i}^{(i)}) = \mathbf{H}(t_0^{(i+1)}), \quad (22)$$

and the two components of the Neumann equation (4) are discretized to

$$\sum_{j=1}^{q_i+1} D_1^{(i)}(q_i+1, j) H_r(t_{j-1}^{(i)}) = \sum_{j=1}^{q_{i+1}+1} D_1^{(i+1)}(1, j) H_r(t_{j-1}^{(i+1)}), \quad (23)$$

$$\sum_{j=1}^{q_i+1} D_1^{(i)}(q_i+1, j) H_\phi(t_{j-1}^{(i)}) = \frac{m(\varepsilon_{r_i^-}/\varepsilon_{r_i^+} - 1)}{r_i} H_r(t_0^{(i+1)}) \\ + \frac{(\varepsilon_{r_i^-}/\varepsilon_{r_i^+} - 1)}{r_i} H_\phi(t_0^{(i+1)}) \\ + \frac{\varepsilon_{r_i^-} - q_{i+1} + 1}{\varepsilon_{r_i^+}} \sum_{j=1}^{q_{i+1}+1} D_1^{(i+1)}(1, j) H_\phi(t_{j-1}^{(i+1)}). \quad (24)$$

Finally, at $r=r_0=t_0^{(1)}$, we get

$$\mathbf{H}(t_0^{(1)}) = 0, \quad m \neq 1, \quad (25)$$

$$\sum_{j=1}^{q_1+1} D_1^{(1)}(1, j) \mathbf{H}(t_{j-1}^{(1)}) = 0, \quad m = 1, \quad (26)$$

and at $r=r_N=t_{q_N}^{(N)}$ there is

$$\mathbf{H}(t_{q_N}^{(N)}) = 0. \quad (27)$$

Those discrete equations for \mathbf{E} formulations are similar to those of \mathbf{H} and are omitted here.

C. The Reformulation of the Matrix Eigenvalue Problem

Let $\mathbf{H}_T = [\mathbf{H}_1^T \ \mathbf{H}_2^T \ \cdots \ \mathbf{H}_N^T]^T$, where \mathbf{H}_i is the column vector in Eq. (19) for $i=1, 2, \dots, N$. A generalized matrix eigenvalue problem,

$$S \mathbf{H}_T = \beta^2 B \mathbf{H}_T, \quad (28)$$

is obtained by assembling the discrete equations (21)–(27) under the sequence of \mathbf{H}_T , where S is a square block sparse coefficient matrix of unknowns and B is the modified identity matrix whose partial principal diagonal elements are replaced with zeros at those boundary and interface nodes.

Huang pointed out in [29] that Eq. (28) can be solved directly by the implicitly restarted Arnoldi method, which is efficient for sparse and large matrices. However, we find that it is more stable and accurate to reduce Eq. (28) to a standard matrix eigenvalue problem.

For conciseness, we take S as a 4×4 matrix to show the detailed procedure. Suppose

$$\begin{bmatrix} s_{11} & s_{12} & s_{13} & s_{14} \\ s_{21} & s_{22} & s_{23} & s_{24} \\ s_{31} & s_{32} & s_{33} & s_{34} \\ s_{41} & s_{42} & s_{43} & s_{44} \end{bmatrix} \begin{bmatrix} H_1 \\ H_2 \\ H_3 \\ H_4 \end{bmatrix} = \beta^2 \begin{bmatrix} 1 & & & \\ & 1 & & \\ & & 0 & \\ & & & 1 \end{bmatrix} \begin{bmatrix} H_1 \\ H_2 \\ H_3 \\ H_4 \end{bmatrix}. \quad (29)$$

If $H_4=0$ is known in Eq. (29), e.g., the zero Dirichlet condition, we can eliminate its corresponding row and column, namely,

$$\begin{bmatrix} s_{11} & s_{12} & s_{13} \\ s_{21} & s_{22} & s_{23} \\ s_{31} & s_{32} & s_{33} \end{bmatrix} \begin{bmatrix} H_1 \\ H_2 \\ H_3 \end{bmatrix} = \beta^2 \begin{bmatrix} 1 & & \\ & 1 & \\ & & 0 \end{bmatrix} \begin{bmatrix} H_1 \\ H_2 \\ H_3 \end{bmatrix}. \quad (30)$$

Furthermore, from the last row of Eq. (30), there is $H_3 = -(s_{31}/s_{33})H_1 - (s_{32}/s_{33})H_2$. Substituting it into the first two rows and doing some simplifications, we get

$$\tilde{S}_{2 \times 2} \begin{bmatrix} H_1 \\ H_2 \end{bmatrix} = \beta^2 \begin{bmatrix} H_1 \\ H_2 \end{bmatrix}. \quad (31)$$

Equation (31) is a standard matrix eigenvalue problem with the eigenvector $[H_1 \ H_2]^T$.

The above elimination process is similar to those done in [14,30], and it can be done locally since S is a block

sparse matrix. After finishing all the recursive eliminations of interface and boundary nodes, we get a standard matrix eigenvalue problem

$$\tilde{S} \begin{bmatrix} \bar{\mathbf{H}}_1 \\ \bar{\mathbf{H}}_2 \\ \vdots \\ \bar{\mathbf{H}}_N \end{bmatrix} = \beta^2 \begin{bmatrix} \bar{\mathbf{H}}_1 \\ \bar{\mathbf{H}}_2 \\ \vdots \\ \bar{\mathbf{H}}_N \end{bmatrix}, \quad (32)$$

where \tilde{S} is the reduction matrix of S and $\bar{\mathbf{H}}_i$ is the column vector in Eq. (20). Equation (32) can be solved by the commonly used matrix eigenvalue solver.

4. NUMERICAL EXAMPLES AND DISCUSSIONS

A. Two Layer Air-Clad Optical Fiber

In this section, several numerical examples are studied to show the validity and performance of our method, of which the solution accuracy and convergence are mainly investigated and compared with other methods.

A two layer ($N=2$) air-clad optical fiber [6] is studied first. Its analytical effective index $n_{\text{eff}} = \beta/\kappa_0$ can be obtained from the nonlinear dispersion relation by the Newton root finding technique [19]. From Fig. 1, the parameters of this fiber are $r_1 = 0.6 \mu\text{m}$ with the core index $n_1 = \sqrt{8}$, and the air cladding index $n_2 = 1.0$ with $r_2 = 6.5 \mu\text{m}$. The PML parameters are $r_{\text{pml}} = 5.0 \mu\text{m}$, $P=4$, $R=10^{-8}$. In fact, as seen in [6], there is no need to use PML here if we are interested only in guiding modes. But the PML is necessary if we also want to compute the leaky modes. To be unified, all the examples studied in this paper are calculated under PMLs.

In this example, the number q_i of the discrete nodes in the i th segment $[r_{i-1}, r_i]$ is determined by

$$q_i = \left\lfloor T \cdot \left(\frac{\alpha_i}{\sum_{i=1}^N \alpha_i} \right) \right\rfloor, \quad i = 1, 2, \quad (33)$$

where T is a given integer, $\lfloor \cdot \rfloor$ denotes the floor, and $\alpha_i = [(r_i - r_{i-1})/r_N] |n_i|$. Suppose that the order of \tilde{S} in Eq. (32) is U , which indicates the number of unknowns.

First, we verify the validity of the MCPS method. The effective index n_{eff} of the fundamental mode HE_{11} of this fiber is shown in Fig. 2 with different wavelengths λ . It can be seen the numerical results (dotted line) obtained by the MCPS method agree well with the exact ones (solid line).

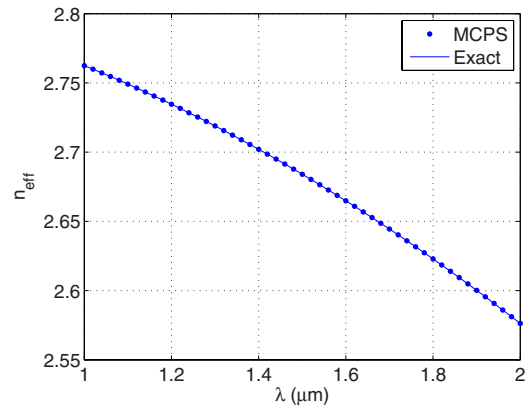


Fig. 2. (Color online) The effective index of the HE_{11} mode for the two layer optical fiber with different λ 's.

Then we study its solution accuracy. Suppose the wavelength $\lambda = 1.5 \mu\text{m}$. The exact effective index of the HE_{11} mode is $n_{\text{eff,exact}} = 2.684\,019\,321\,601\,08$ [6]. In Table 1, we show the numerical n_{eff} obtained by both the electric and magnetic formulations. It can be seen the numerical n_{eff} achieves up to 12 digits when $U=114$ and the solution results of the two formulations are almost the same. By comparison, similar precision (11 digits) of n_{eff} was achieved in PSFD [6] with 4840 unknowns. Correspondingly, the computing time of MCPS at $U=114$ is only 0.1825 s on a personal computer with an Intel Pentium 4 3.0 GHz central processing unit (CPU), while that of the PSFD [6] takes more than 52 s with an Intel Dual Core 4300 1.8 GHz CPU. Obviously, the 1-D MCPS method is more efficient compared to the 2-D PSFD method in [6] for the circular waveguide.

Finally, we consider the convergence of the MCPS method. The relative error is defined by

$$\text{Relative error} = \frac{|n_{\text{eff}} - n_{\text{eff,exact}}|}{|n_{\text{eff,exact}}|}, \quad (34)$$

where n_{eff} is the numerical effective index. In Fig. 3, the convergence curves of the MCPS method are shown to compare with that of the FD method in [4]. It can be seen that our MCPS method converges much faster and the performances of its H and E formulations are identical. Actually, the FD method in [4] has $O(h^2)$ convergence rate, where $h = (r_N - r_0)/K$ is the step size with K as the number of discrete nodes. But the spectral methods usually have the typical convergence rate $O(c^K)$ ($0 < c < 1$) to approximate the analytical functions [14]. Thus, to reach the same precision, the number of nodes needed in MCPS is much less than the FD in [4]. On the other hand, if the

Table 1. The Numerical n_{eff} of HE_{11} Mode ($m=1$) by MCPS for Air-Clad Optical Fiber

T	U	$n_{\text{eff}}(\mathbf{E})$	$n_{\text{eff}}(\mathbf{H})$
10	14	2.710 234 122 200 30-7.85 $\times 10^{-7}i$	2.710 234 122 200 30-7.85 $\times 10^{-7}i$
20	34	2.684 394 856 970 74+3.11 $\times 10^{-8}i$	2.684 394 856 970 74+3.11 $\times 10^{-8}i$
30	54	2.684 023 848 731 34+6.33 $\times 10^{-10}i$	2.684 023 848 731 34+6.33 $\times 10^{-10}i$
40	74	2.684 019 330 566 38+1.75 $\times 10^{-12}i$	2.684 019 330 566 40+1.75 $\times 10^{-12}i$
50	94	2.684 019 321 620 47	2.684 019 321 620 47
60	114	2.684 019 321 608 19	2.684 019 321 608 18

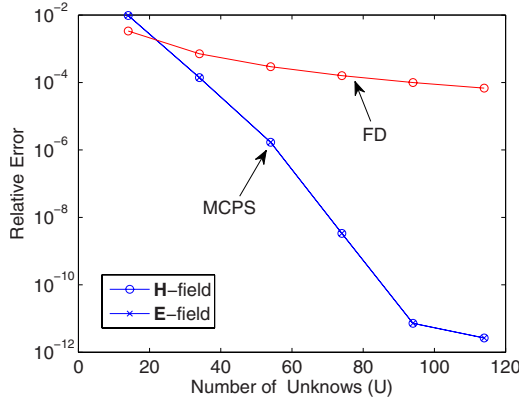


Fig. 3. (Color online) The convergence curves of the HE_{11} mode by MCPS compared with the FD in [4] for the air-clad optical fiber.

same number of nodes are used, a much higher order of accuracy can be obtained by MCPS.

B. The Optical Fiber Hybrid Surface Plasmon Polariton

We study the optical fiber hybrid SPP [4,20] here to verify the effectiveness of the MCPS method for circular waveguides in lossy materials. A typical hybrid SPP is composed of three different layers ($N=3$) of materials. As seen in Fig. 1, the core index $n_1=1.515$ and the core radius r_1 satisfy $\kappa_0 r_1=5.0$. The second layer is silver with the relative permittivity $\epsilon_r=-19+0.53i$ ($n_2=\epsilon_r^{1/2}$) at the wavelength of $\lambda=0.6328 \mu\text{m}$, and r_2 satisfies $\kappa_0(r_2-r_1)=0.6$. The index of the cladding layer is $n_3=1.500$ and $r_3=r_{\text{pml}}+d \mu\text{m}$. The PML parameters are same as the two layer fiber studied before except $r_{\text{pml}}=6.0 \mu\text{m}$.

Since the thin metal layer of the hybrid SPP has significant influence on the effective index, the node distribution in this layer must be denser than the other two layers. In this example, the node number q_i of the i th segment $[r_{i-1}, r_i]$ is determined by

$$q_i = \lceil T\alpha_i \rceil, \quad i = 1, 2, 3, \quad (35)$$

where T is a given integer, $\lceil \cdot \rceil$ denotes the ceil, and $\alpha = [0.147 \ 0.118 \ 0.735]$.

When $m=4$, the analytical n_{eff} of the antisymmetric mode is $1.506444 + 3.663 \times 10^{-3}i$ [20]. It was also solved as $1.506444 + 3.662701 \times 10^{-3}i$ by the FD method in [4]. In Table 2, we compute it by MCPS with different T 's under the PML parameters $d=1.0 \mu\text{m}$ and $R=10^{-8}$. It can be seen n_{eff} of MCPS at $T=60$ has similar accuracy as that of the FD method. Since the MCPS solutions converge, n_{eff} at $T=120$ is certainly more accurate than $T=60$. To make sure of its reachable digits, a high-precision reference so-

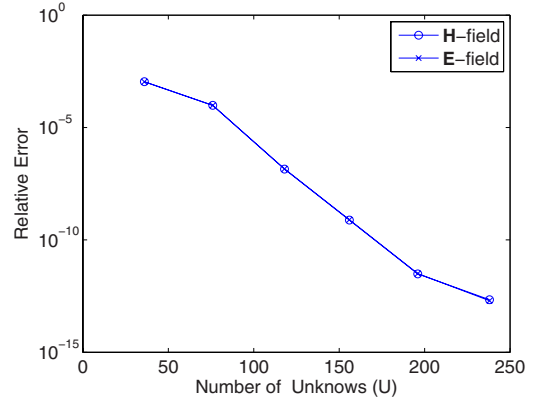


Fig. 4. (Color online) The convergence curves of the antisymmetric mode ($m=4$) by MCPS for hybrid SPP.

lution is needed. We compute it through the MCPS method with enough nodes. In fact, $T=200$ and $T=300$ under the following PML parameters:

- $R=10^{-8}$ and $d=0.2j \mu\text{m}$, $j=1, 2, \dots, 10$;
- $R=10^{-12}$ and $d=0.2j \mu\text{m}$, $j=1, 2, \dots, 10$;
- $d=1.0 \mu\text{m}$ and $R=10^{-2j}$, $j=2, 3, \dots, 7$,

are considered. In this way, we obtain the credible n_{eff} of the antisymmetric mode ($m=4$) as $1.5064437413 + 3.662698058 \times 10^{-3}i$. Thus, the results of the antisymmetric mode ($m=4$) in Table 2 are believed to have eleven exact digits in real part and ten accurate digits in imaginary part.

Finally, we consider the convergence rate of the MCPS method for this example. Let the MCPS result with $T=200$ ($U=396$) be the reference solution. The PML parameters are fixed as $d=1 \mu\text{m}$ and $R=10^{-8}$. This is because other PML parameters lead to similar convergence results. In Fig. 4, we observe the spectral convergence behavior, where the smallest relative error achieves $O(10^{-12})$ at $U=238$. The convergence rates of the two formulations are almost identical.

C. The Bragg Fibers

The Bragg fibers [4,22–24] attract more and more attention due to their special properties of guiding light. They are studied here to show the performance of the MCPS method in the super-multi-interface structures. As known, a typical hollow core Bragg fiber is composed of an air-core, several periodic pairs of alternating materials, and an outmost infinite cladding layer.

The parameters of two Bragg fibers [4,24] are introduced in Table 3, where n_1 is the air-core index; n_2 and n_3 are, respectively, the high and low indices of the first pe-

Table 2. The Numerical n_{eff} of Antisymmetric Mode ($m=4$) by MCPS for Hybrid SPP

T	U	$n_{\text{eff}}(\mathbf{E})$	$n_{\text{eff}}(\mathbf{H})$
20	36	$1.504873354739528 + 4.079641634744 \times 10^{-3}i$	$1.50484365258878 + 4.076213008938 \times 10^{-3}i$
40	76	$1.506299567238919 + 3.665911796684 \times 10^{-3}i$	$1.506297785778939 + 3.665763504535 \times 10^{-3}i$
60	118	$1.506443523479754 + 3.662701351070 \times 10^{-3}i$	$1.506443527907785 + 3.662701557772 \times 10^{-3}i$
80	156	$1.506443740128931 + 3.662698102403 \times 10^{-3}i$	$1.506443740170344 + 3.662698103466 \times 10^{-3}i$
100	196	$1.506443741314853 + 3.662698058128 \times 10^{-3}i$	$1.506443741314997 + 3.662698058130 \times 10^{-3}i$
120	238	$1.506443741319942 + 3.662698058103 \times 10^{-3}i$	$1.506443741319974 + 3.662698058102 \times 10^{-3}i$

Table 3. Parameters of two Bragg Fibers

ID	n_1	n_2	n_3	n_N	r_1 (μm)	δ_1 (μm)	δ_2 (μm)	N_{pair}	N
(a)	1.0	1.49	1.17	1.49	1.3278	0.2133	0.3460	16	34
(b)	1.0	1.45	1.10	1.45	2.0	0.5	0.5	50	102

Table 4. The Numerical n_{eff} of TE_{01} Mode ($m=0$) by MCPS for Bragg Fiber (a)

T	U	$n_{\text{eff}}(\mathbf{E})$	$n_{\text{eff}}(\mathbf{H})$
200	346	0.891 692 470 534 612–1.224 474 1 $\times 10^{-8}i$	0.891 692 470 534 627–1.224 473 9 $\times 10^{-8}i$
300	568	0.891 062 513 765 067–1.426 342 3 $\times 10^{-8}i$	0.891 062 513 765 046–1.426 342 7 $\times 10^{-8}i$
400	758	0.891 066 997 011 825–1.422 152 0 $\times 10^{-8}i$	0.891 066 997 011 910–1.422 152 1 $\times 10^{-8}i$
500	980	0.891 067 218 043 187–1.422 606 8 $\times 10^{-8}i$	0.891 067 218 043 118–1.422 607 2 $\times 10^{-8}i$
600	1170	0.891 067 217 430 514–1.422 605 2 $\times 10^{-8}i$	0.891 067 217 430 386–1.422 605 5 $\times 10^{-8}i$
700	1360	0.891 067 217 466 421–1.422 604 9 $\times 10^{-8}i$	0.891 067 217 466 790–1.422 604 7 $\times 10^{-8}i$

Table 5. The n_{eff} of Higher Order Modes of Bragg Fiber (a) Calculated by Different Methods

	TM_{01} ($m=0$)	Hybrid ($m=1$)
MCPS ($T=700$)	0.792 085 903 112 979–1.819 323 186 129 $\times 10^{-3}i$	0.805 577 881 426 740–1.739 146 908 714 $\times 10^{-3}i$
Improved FD [4]	0.792 095–1.8191 $\times 10^{-3}i$	0.805 582–1.7389 $\times 10^{-3}i$
FD frequency domain [2]	N/A	0.805 583–1.7375 $\times 10^{-3}i$
Chew's method [31]	0.792 086–1.8190 $\times 10^{-3}i$	0.805 578–1.7392 $\times 10^{-3}i$

riodic pair of materials in the second and third layers; n_N is the index of the outmost infinite cladding layer; r_1 is the core radius; δ_1 ($=r_2-r_1$) and δ_2 ($=r_3-r_2$) are, respectively, the thicknesses of the second and third layers; N_{pair} is the number of periodic pairs; and N ($=2N_{\text{pair}}+2$) is total number of layers (see Fig. 1). The outmost infinite cladding layers of the two fibers are truncated by PMLs with $r_{\text{pml}}=r_1+N_{\text{pair}}(\delta_1+\delta_2)+5 \mu\text{m}$ and $r_N=r_{\text{pml}}+d \mu\text{m}$.

In the two examples, the node number q_i of the i th segment $[r_{i-1}, r_i]$ is determined by the following rule:

$$q_i = \left\lceil T \left(\frac{\alpha_i}{N} \right) \right\rceil, \quad i = 1, 2, \dots, N, \quad (36)$$

$$\alpha_i = \left\lceil (r_i - r_{i-1}) / r_N \right\rceil n_i.$$

where T is a given integer, $\lceil \cdot \rceil$ denotes the ceil, and $\alpha_i = \lceil (r_i - r_{i-1}) / r_N \rceil n_i$.

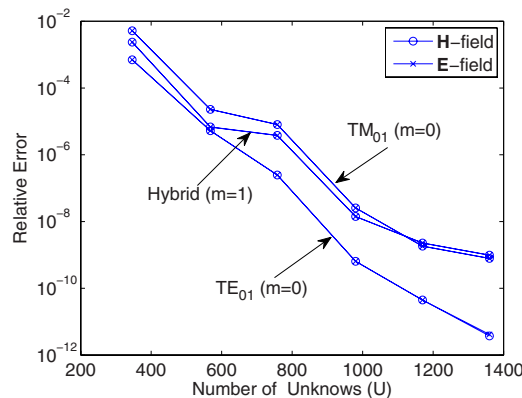


Fig. 5. (Color online) The convergence curves of the modes by MCPS for Bragg fiber (a).

Different from the two layer fiber studied before, the fundamental mode of the Bragg fiber is the TE_{01} mode and it has the lowest loss compared to other higher order modes. Suppose the wavelength $\lambda=1.0 \mu\text{m}$. For Bragg fiber (a), n_{eff} of its fundamental mode was solved as $0.891 068-1.4227 \times 10^{-8}i$ in [4] by the FD method. Another earlier result was $0.891 067-1.4226 \times 10^{-8}i$ by Chew's method [31]. In Table 4, we show our MCPS results under the PML parameters $d=1.0 \mu\text{m}$ and $R=10^{-8}$. It can be seen that the MCPS solutions are closer to those of Chew's method [31]. In order to make sure of the reachable digits, we use the same method as the hybrid SPP but with $T=1200$ to compute the reference solutions for the modes of Bragg fiber (a). In this way, we obtain the credible n_{eff} of the TE_{01} mode as $0.891 067 217 4-1.422 60 \times 10^{-8}i$. Thus, the MCPS results in Table 4 with $T=700$ are believed to have ten accurate digits in real part and six exact digits in imaginary part. To achieve

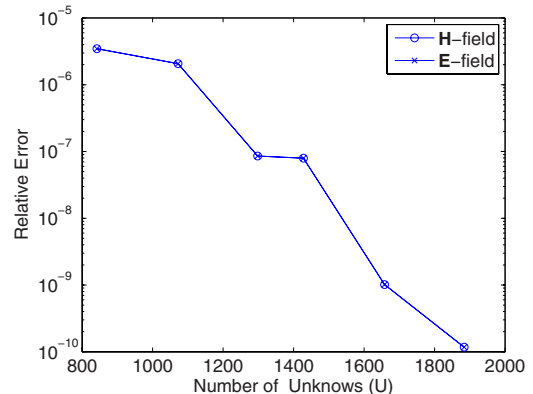


Fig. 6. (Color online) The convergence curves of the TE_{01} mode ($m=0$) by MCPS for Bragg fiber (b).

Table 6. The Propagation Constant β of the TE₀₁ Mode ($m=0$) by MCPS for Bragg Fiber (b)

T	U	$\beta(\mathbf{E})$	$\beta(\mathbf{H})$
500	842	2.512 645 016 906 381+ $1.1 \times 10^{-14}i$	2.512 645 016 906 348+ $4.0 \times 10^{-15}i$
600	1072	2.512 648 540 225 474- $1.9 \times 10^{-14}i$	2.512 648 540 225 040- $1.9 \times 10^{-14}i$
700	1298	2.512 653 950 400 662- $2.2 \times 10^{-14}i$	2.512 653 950 400 798+ $7.0 \times 10^{-15}i$
800	1428	2.512 653 535 595 115+ $1.7 \times 10^{-14}i$	2.512 653 535 595 069- $8.0 \times 10^{-15}i$
900	1658	2.512 653 737 717 467- $3.5 \times 10^{-14}i$	2.512 653 737 717 334- $1.1 \times 10^{-14}i$
1000	1884	2.512 653 735 463 200- $1.0 \times 10^{-15}i$	2.512 653 735 463 253+ $4.4 \times 10^{-14}i$

similar precision as the FD result, only eight nodes in the thinner δ_1 layer are needed in MCPS ($T=500$), while it is 100 for that of the FD in [4]. So it indicates again that the MCPS converges much faster than the FD method.

Other higher order modes such as the TM₀₁ ($m=0$) and the hybrid ($m=1$) modes are also calculated by MCPS for Bragg fiber (a). To be concise, only n_{eff} at $T=700$ with the PML parameters $d=1.0 \mu\text{m}$ and $R=10^{-8}$ is shown and compared with the known results in Table 5. Good agreement is observed on these data. The reference solutions of these two modes are also computed in the same way as the TE₀₁ mode. The credible effective index of TM₀₁ mode is 0.792 085 903-1.819 322 $\times 10^{-3}i$. It can be seen that the MCPS result with $T=700$ has nine exact digits in real part and six exact digits in imaginary part. Similarly, the credible n_{eff} of the hybrid mode ($m=1$) is 0.805 577 881-1.739 146 $\times 10^{-3}i$. Thus, the result of the hybrid mode in Table 5 has nine exact digits in real part and seven accurate digits in imaginary part.

Then we study the convergence rates of MCPS to solve these three modes. The reference solutions are all obtained by MCPS at $T=1200$ ($U=2374$). The PML parameters are fixed as $d=1 \mu\text{m}$ and $R=10^{-8}$. The convergence curves are shown in Fig. 5, where the spectral convergence is observed. Particularly, the convergence rate of the TE₀₁ mode is a little faster than the other two modes. It indicates that more nodes are needed in the higher order modes than the fundamental mode if the same order of precision is desired.

The Bragg fiber (b) [24] has more periodic pairs than the Bragg fiber (a). Suppose the wavelength $\lambda=2.0 \mu\text{m}$. The analytical propagation constant of the TE₀₁ mode of Bragg fiber (b) is $\beta_{\text{exact}}=2.512 653 735 168 542$ [24]. Suppose that the PML parameters are fixed as $d=1 \mu\text{m}$ and $R=10^{-8}$. In Table 6, we show the numerical results of β by the MCPS method. The imaginary parts of β are on the order of 10^{-14} , which indicates that the TE₀₁ mode is a quasi-guided mode with a very low loss. When $T=1000$, nine accurate digits after the decimal point are obtained, while only eight nodes are used in the δ_2 layer. The convergence curve of the TE₀₁ mode for Bragg fiber (b) is shown in Fig. 6, where the quasi-spectral convergence is observed.

5. CONCLUSION

We have proposed a new 1-D full-vectorial mode solver based on the multidomain Chebyshev pseudospectral (MCPS) method for the circular waveguides. Numerical studies have verified its validity and performance. We see

that the MCPS solutions have quasi-spectral convergence rate and they agree well with the known results. Particularly, compared to the FD method in [4], a much higher order of solution accuracy is achieved in the MCPS method with even less nodes. And the MCPS method is also more efficient than the PSFD method in [6] due to its lower dimension advantage. In addition, the indiscernible difference on the performance of the electric and magnetic MCPS formulations shows its self-consistency. Although the MCPS method is described only for step-index circular optical waveguides in this paper, we also indicate that it can be easily extended to the graded index ones if we replace the constant $\kappa_0^2 \epsilon_r$ with $\kappa_0^2 \epsilon_r(t_k^{(i)})$ in the discrete equations.

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